On Track: Path Following Controller Designs for Autonomous and Semi-Autonomous Industrial Motor Graders

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Introduction

This paper introduces **Single Track Control** (STC), a control methodology that enables existing automation techniques for centre-articulated vehicles to be applied to industrial motor graders.

Motor Graders are heavy machinery used to smooth, or grade, road surfaces at mine sites with a moldboard (blade). This operation is crucial for **mine safety** and **efficiency**. However, complex terrain interactions, 6–DoF moldboard control, and **redundant steering kinematics** resulting from frame articulation and front wheel steering have complicated automation efforts.

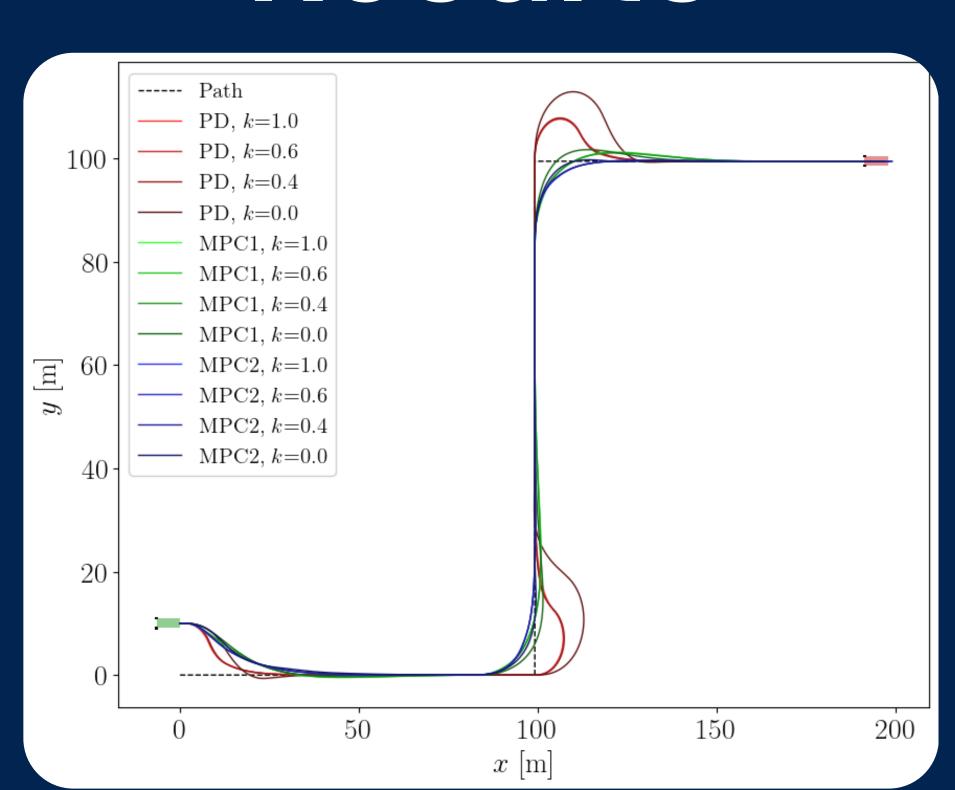
Single Track Control leverages the redundancy to impose that the rear wheels follow the same track (path) as the front wheels, like other centrearticulated mining vehicles – i.e. Load Haul Dump (LHD) or haulage trucks.

We designed STC-enabled controllers, and performed a tuning analysis in simulation to assess viability of the methodology as proof-of-concept.





Results



Selected controller comparison. Error was measured as RMSE of path following errors; effort was measured as the L² norm of rate inputs.

Controller	$k_{ m STC}$	Parameters	RMSE	Effort
FBL+PD	0.0	$\omega_n = 1.63, \zeta = 1.03$	1310	6.19
STC+FBL+PD	1.0	$\omega_n = 1.63, \zeta = 1.03$	668	5.50
FBL+MPC1	0.0	q = 22.7, r = 1.89	580	2.97
STC+FBL+MPC1	0.4	q = 11.4, r = 4.29	614	2.34
FBL+MPC2	0.0	q = 2.16, r = 4.78	465	3.35
STC+FBL+MPC2	1.0	q = 0.239, r = 5.19	477	2.46

A tuning analysis was done to analyze the performance of STC-enabled controllers (one PD, two MPC). Results indicate that comparable path-following performance, with reduced actuator effort in all cases, indicating promise for field applications.

Future work includes addressing the plant-model mismatch, simulation under dynamic disturbances, and field experiments.

Benefits of STC

Practically, STC presents three main benefits:

1) improved safety and manoeuvrability for navigating underground drifts,

2) existing techniques for centre-articulated vehicles can be extended to **autonomous** operation of motor graders, and

3) STC consolidates steering as a single input, reducing the need for specialized training in **semi-autonomous** applications.

[1] A. Beca and J. A. Marshall, "Path following controller designs for autonomous and semi-autonomous industrial motor graders," Proc. Conf. Robots and Vision (CRV), Calgary, AB, Canada, 2025
[2] J. A. Marshall, T. D. Barfoot, and J. Larsson, "Autonomous underground tramming for center-articulated vehicles," J. Field Robot., vol. 25, no. 6-7, pp. 400–421, Jun. 2008.

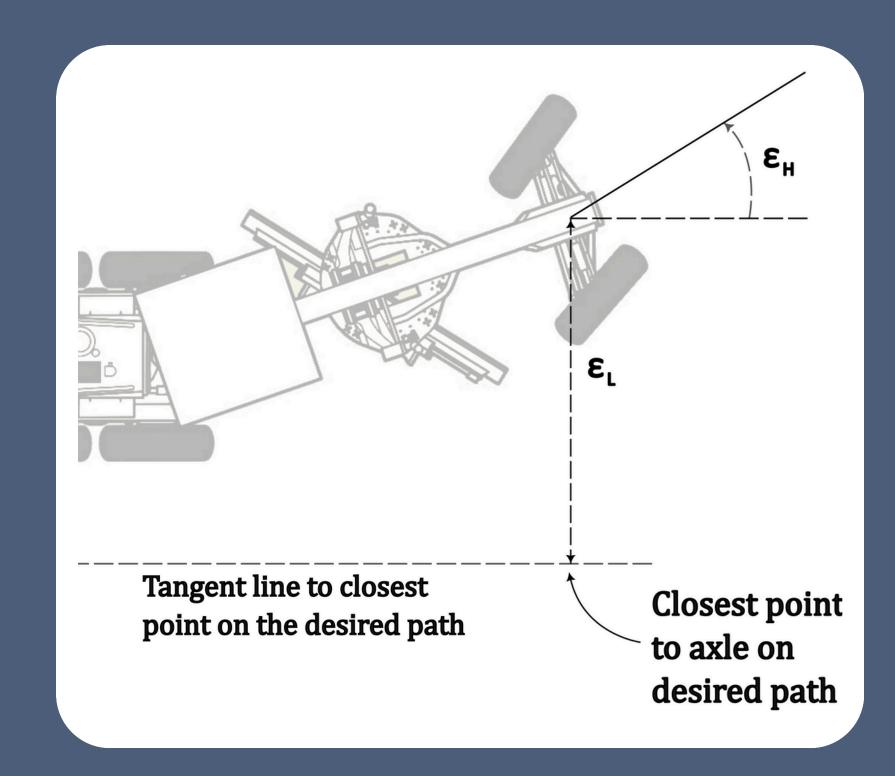
Control Design

We derive **vehicle kinematics**, and apply extend existing techniques to evaluate **feedback linearized + single track controllers (FBL+STC)**. To resolve kinematic redundancy, we:

 v_1 : maintain a constant linear speed

 v_2 : obtain desired articulation rate with an **FBL controller** (PD, 2x MPC), [2]

 v_3 : solve for the corresponding steering angle to satisfy **STC**

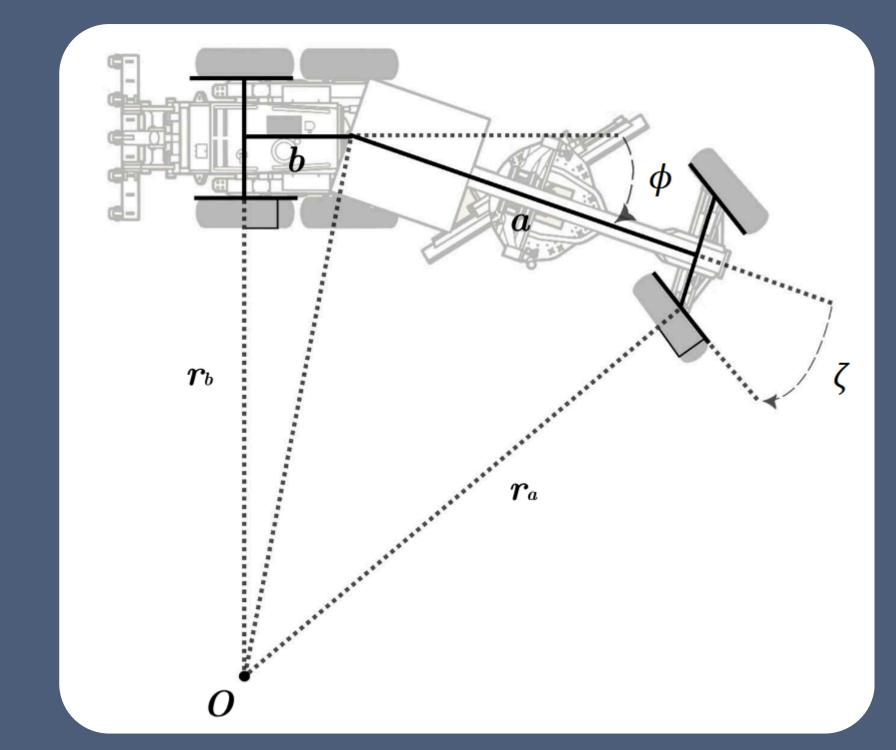


We define lateral and heading errors for the front wheels, and chain for the FBL error system

$$\begin{bmatrix} \dot{z}_1 \\ \vdots \\ z_2 \end{bmatrix} = \begin{bmatrix} \dot{\varepsilon}_L \\ \vdots \\ \varepsilon_L \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} \mathbf{z} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} \boldsymbol{\eta}$$

then unwarp FBL input η for articulation rate v_2 ,

$$v_2 = \frac{b}{a\cos(\phi) + b} \left(\frac{\eta}{v_1\cos(\varepsilon_H)}\right)$$



With ϕ_d selected by FBL, we choose ζ such that $r_a = r_b$, obtaining

$$\frac{b}{a} = \frac{\cos(\phi) - \cos(\zeta)}{\cos(\phi + \zeta) - 1}$$

A 1st order controller tracks ζ_d , varying the effect of the plant-model mismatch.

Note: STC is not separable; a numerical method is used to converge to a solution.

